

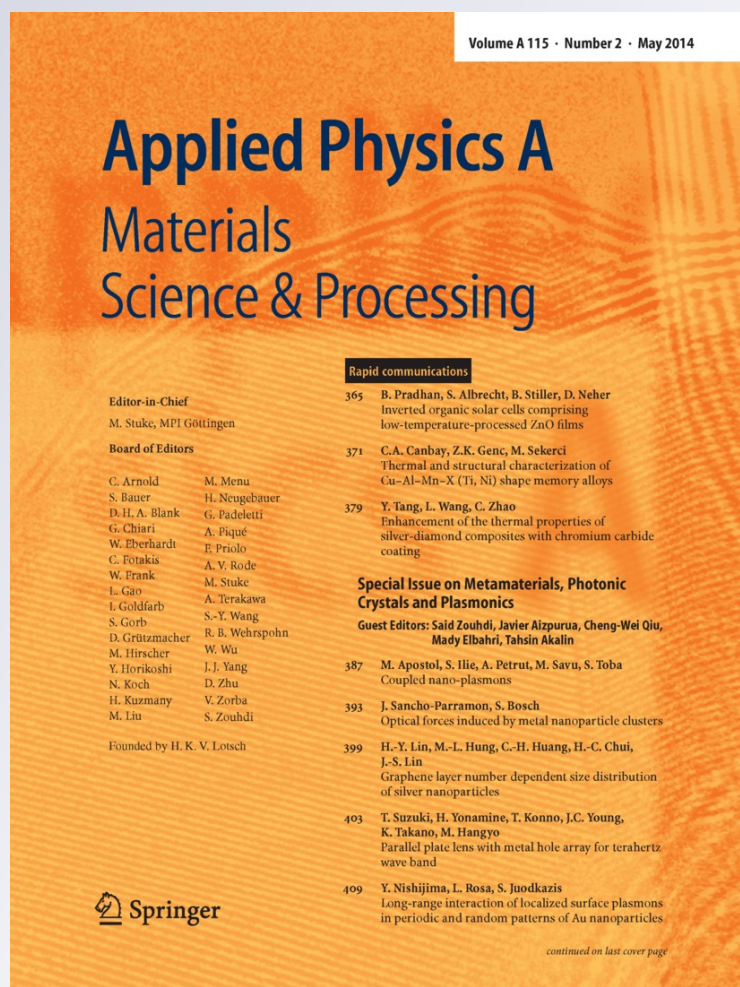
# $\mathcal{PT}$ -symmetric nonlinear metamaterials and zero-dimensional systems

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# $\mathcal{PT}$ -symmetric nonlinear metamaterials and zero-dimensional systems

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**Abstract** A one dimensional, parity-time ( $\mathcal{PT}$ )-symmetric magnetic metamaterial comprising split-ring resonators having both gain and loss is investigated. In the linear regime, the transition from the exact to the broken  $\mathcal{PT}$ -phase is determined through the calculation of the eigenfrequency spectrum for two different configurations; the one with equidistant split-rings and the other with the split-rings forming a binary pattern ( $\mathcal{PT}$  dimer chain). The latter system features a two-band, gapped spectrum with its shape determined by the gain/loss coefficient as well as the interelement coupling. In the presence of nonlinearity, the  $\mathcal{PT}$  dimer chain configuration with balanced gain and loss supports nonlinear localized modes in the form of a novel type of discrete breathers below the lower branch of the linear spectrum. These breathers that can be excited from a weak applied magnetic field by frequency chirping, can be subsequently driven solely by the gain for very long times. The effect of a small imbalance between gain and loss is also considered. Fundamental gain-driven breathers occupy both sites of a dimer, while their energy is almost equally partitioned between the two split-rings, the one with gain and the other with loss. We also introduce a model equation for the investigation of classical  $\mathcal{PT}$  symmetry in zero dimensions, realized by a simple harmonic oscillator with matched time-dependent gain and loss that exhibits a transition from oscillatory to diverging motion. This behavior is similar to a

transition from the exact to the broken  $\mathcal{PT}$  phase in higher-dimensional  $\mathcal{PT}$ -symmetric systems. A stability condition relating the parameters of the problem is obtained in the case of a piece-wise constant gain/loss function that allows the construction of a phase diagram with alternating stable and unstable regions.

## 1 Introduction

The investigation of artificial materials whose properties can be tailored has recently attracted a lot of attention. Considerable research effort has been invested in the development of artificial structures that exhibit properties not found in nature. Two recent and well-known paradigms are the metamaterials that provide full access to all four quadrants of the real permittivity–permeability plane [39], and the parity-time ( $\mathcal{PT}$ ) symmetric systems, whose properties rely on a delicate balance between gain and loss. The latter belong to a class of “synthetic” materials that do not obey separately the parity ( $\mathcal{P}$ ) and time ( $\mathcal{T}$ ) symmetries, but instead they do exhibit a combined  $\mathcal{PT}$  symmetry. The ideas and notions of  $\mathcal{PT}$ -symmetric systems have their roots in quantum mechanics where  $\mathcal{PT}$ -symmetric Hamiltonians have been studied for many years [13]. The notion of  $\mathcal{PT}$  symmetry has been recently extended to dynamical lattices, particularly in optics, where photonic lattices combining gain and loss elements offer new possibilities for shaping optical beams and pulses. Soon after the development of the theory of  $\mathcal{PT}$ -symmetric optical lattices [7, 22], the  $\mathcal{PT}$ -symmetry breaking was experimentally observed [11, 28, 35]. Naturally, such considerations have also been extended to nonlinear lattices [6, 23] and oligomers [20], and  $\mathcal{PT}$ -related phenomena like unidirectional optical transport [26], unidirectional invisibility [21], and Talbot effects [25] were theoretically

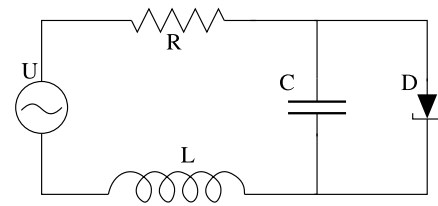
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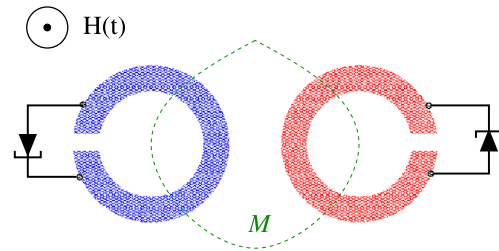
investigated. Moreover, it has been shown that optical solitons [1, 2, 6, 33], nonlinear modes [38], and breathers [4, 19] may also be supported by  $\mathcal{PT}$ -symmetric systems. Moreover, the application of these ideas in electronic circuits [30], not only provides a platform for testing  $\mathcal{PT}$ -related ideas within the framework of easily accessible experimental configurations, but also provides a direct link to metamaterials whose elements can be modeled with equivalent electrical circuits.

Conventional metamaterials comprising resonant metallic elements operate close to their resonance frequency where unfortunately the losses are intolerably high and hamper any possibility for their use in device applications. The pathways to overcome losses are either to replace the metallic parts with superconducting ones [3] or to construct active metamaterials by incorporating active constituents that provide gain through external energy sources. The latter has been recently recognized as a very promising technique for compensating losses [5, 32]. A particular electronic component that may provide both gain and nonlinearity in a metamaterial is the tunnel (Esaki) diode, which features a current-voltage characteristic with a negative resistance part [8]. Left-handed transmission lines with successful implementation of Esaki diodes have been recently realized [14], although other electronic components may be employed as well for loss compensation [37]. Thus, the fabrication of  $\mathcal{PT}$ -symmetric metamaterials with balanced gain and loss is feasible with the present technology in the microwaves, combining highly conducting split-ring resonators (SRRs) and negative resistance devices in a way similar to that in electrical circuits [30]. In this prospect, the SRR equivalent circuit parameters and the bias of the negative resistance device should be properly adjusted to provide gain and equal amount of loss as well as real eigenfrequencies in a finite frequency range of the gain/loss parameter.

In the following, we present a one-dimensional, discrete, equivalent circuit model for an array of SRRs with alternating gain and loss in the two different configurations (Sect. 2). In Sect. 3, we present linear eigenfrequency spectra for systems with small number of SRRs and obtain the expression that provides the eigenfrequencies for large systems. It is shown that  $\mathcal{PT}$ -symmetric metamaterials undergo spontaneous symmetry breaking from the exact  $\mathcal{PT}$  phase (real eigenfrequencies) to the broken  $\mathcal{PT}$  phase (at least one pair of complex eigenfrequencies), with variation of the gain/loss coefficient. In Sect. 4, where nonlinearity becomes important, the generation of long-lived nonlinear excitations in the form of discrete breathers (DBs) [10] is demonstrated numerically. These novel gain-driven DBs result by a purely dynamical process, through the matching of the input power due to gain and internal loss. In Sect. 5, we introduce a model  $\mathcal{PT}$ -symmetric system in zero dimensions, realized by a harmonic oscillator with balanced time-periodic gain



**Fig. 1** Electrical equivalent circuit for a split-ring resonator loaded with a tunnel (Esaki) diode



**Fig. 2** Schematic of a  $\mathcal{PT}$ -symmetric metadimer comprising two tunnel diode-loaded SRRs in an alternating magnetic field  $H(t)$ . The SRRs are coupled magnetically through their mutual inductance  $M$ . Different bias in the diodes may create a balanced gain/loss structure

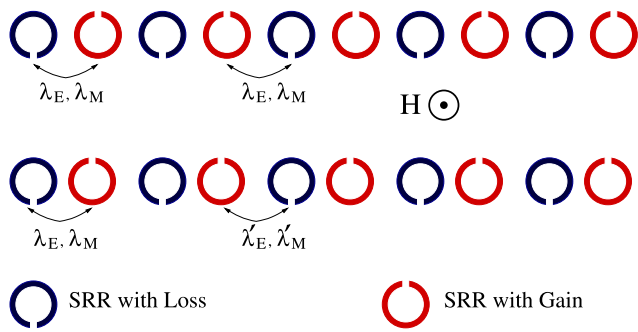
and loss that exhibits extraordinary properties and multiple critical (phase transition) points. Section 6 contains the conclusions.

## 2 Equivalent circuit modelling and dynamic equations

Consider a metallic split-ring resonator (SRR) that can be regarded as an  $RLC$  electrical circuit featuring Ohmic resistance  $R$ , inductance  $L$ , and capacitance  $C$ . A tunnel (Esaki) diode [8] is connected in parallel with the capacitance  $C$  of the SRR (Fig. 1) forming thus a nonlinear metamaterial element with gain. Esaki diodes exhibit a well-defined negative resistance region in their current-voltage characteristics that has a characteristic 'N' shape. A bias voltage applied to the diode can move its operation point in the negative resistance region and then the SRR-diode system gains energy from the source.

A metadimer comprising two SRRs loaded with tunnel diodes in an external alternating magnetic field is shown in Fig. 2. The equivalent circuit parameters  $R$ ,  $C$ , and  $L$  of the SRRs and the bias in the diodes have been adjusted so that: (i) the two elements have the same eigenfrequencies and (ii) one of the SRRs has gain while the other has equal amount of loss. Then the pair of SRRs is a  $\mathcal{PT}$ -symmetric metadimer that may be employed for the construction of one-dimensional  $\mathcal{PT}$ -symmetric metamaterials, which moreover are nonlinear due to the tunnel diodes. The alternating magnetic field induces an electromotive force in each SRR due to Faraday's law, which in turn produce currents that couple the SRRs magnetically





**Fig. 3** Schematic of a one-dimensional  $\mathcal{PT}$ -symmetric metamaterial. *Upper panel*: all the SRRs are equidistant. *Lower panel*: the separation between SRRs is modulated according to a binary pattern ( $\mathcal{PT}$  dimer chain). The applied field is such that the magnetic component is perpendicular to the plane of the split-ring resonators

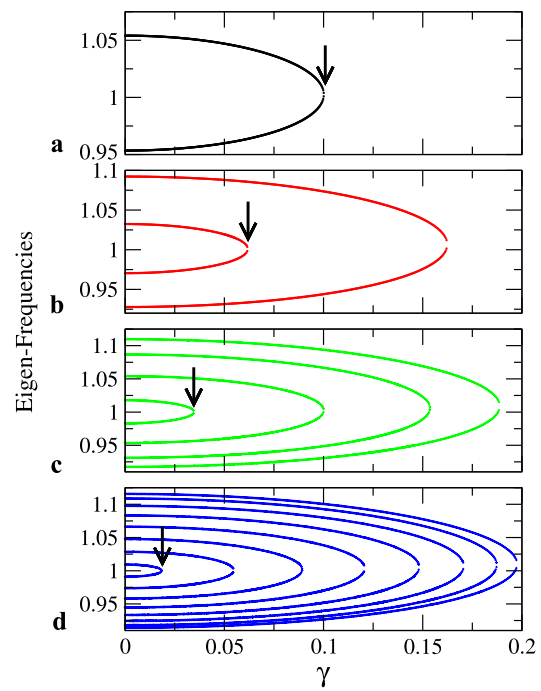
through their mutual inductance  $M$  (Fig. 2). The coupling strength between SRRs is rather weak due to the nature of their interaction (magnetoinductive), and has been calculated accurately by several authors [27, 34]. The SRRs may also be coupled electrically, through the electric dipoles that develop in their slits. Thus, in the general case one has to consider both magnetic and electric coupling between SRRs. However, for particular relative orientations of the SRR slits, the magnetic interaction is dominant, while the electric interaction can be neglected in a first approximation [9, 12, 31]. As can be seen in Fig. 3, the  $\mathcal{PT}$ -symmetric metadimers can be arranged in a one-dimensional lattice in two distinct configurations; one with all the SRRs equidistant and the other with the SRRs forming a  $\mathcal{PT}$  dimer chain.

Within the framework of the equivalent circuit model, a set of discrete differential equations have been used to describe the dynamics in nonlinear magnetic metamaterials [15, 18, 24, 27]. Taking into account the binary structure of the  $\mathcal{PT}$  dimer chain, the dynamics of the  $\mathcal{PT}$ -symmetric metamaterial with balanced gain and loss is governed by the equations [19] (in normalized form)

$$\lambda'_M \ddot{q}_{2n} + \ddot{q}_{2n+1} + \lambda_M \ddot{q}_{2n+2} + \lambda'_E q_{2n} + q_{2n+1} + \lambda_E q_{2n+2} + \alpha q_{2n+1}^2 + \beta q_{2n+1}^3 + \gamma \dot{q}_{2n+1} = \varepsilon_0 \sin(\Omega \tau) \quad (1)$$

$$\lambda_M \ddot{q}_{2n-1} + \ddot{q}_{2n} + \lambda'_M \ddot{q}_{2n+1} + \lambda_E q_{2n-1} + q_{2n} + \lambda'_E q_{2n+1} + \alpha q_{2n}^2 + \beta q_{2n}^3 - \gamma \dot{q}_{2n} = \varepsilon_0 \sin(\Omega \tau) \quad (2)$$

where  $\lambda_M, \lambda'_M$ , and  $\lambda_E, \lambda'_E$  are the magnetic and electric coupling coefficients, respectively, with  $\lambda_{E,M} > \lambda'_{E,M}$  and  $\lambda_{E,M} \lambda'_{E,M} > 0$ ,  $\alpha$  and  $\beta$  are dimensionless nonlinear coefficients,  $\gamma$  is the gain/loss coefficient ( $\gamma > 0$ ),  $\varepsilon_0$  is the amplitude of the external driving voltage, while  $\Omega$  and  $\tau$  are the driving frequency and temporal variable, respectively, normalized to the inductive-capacitive ( $LC$ ) resonance frequency  $\omega_0$  and inverse  $LC$  resonance frequency  $\omega_0^{-1}$ , respectively,  $\omega_0 = 1/\sqrt{LC_0}$  with  $C_0$  being the linear capacitance. The values selected for the nonlinear coefficients

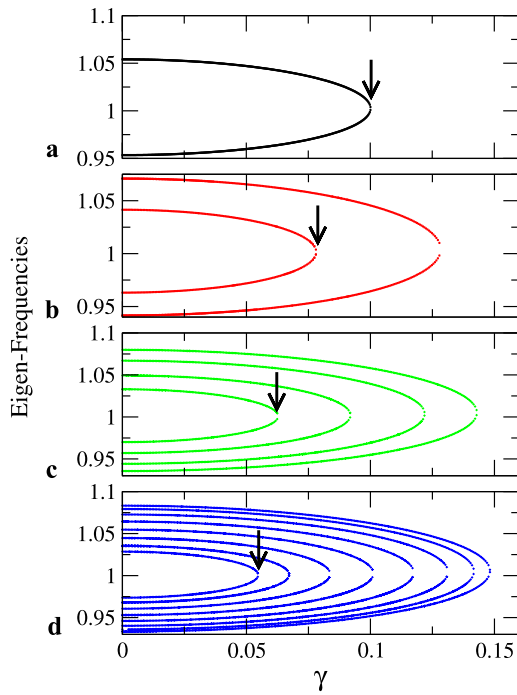


**Fig. 4** Frequency eigenvalues of the free  $\mathcal{PT}$ -symmetric SRR array as a function of the gain/loss parameter  $\gamma$  for  $\lambda_E = 0$ ,  $\lambda_M = -0.1$ , and (a)  $N = 2$ ; (b)  $N = 4$ ; (c)  $N = 8$ ; (d)  $N = 16$ . The arrows indicate the critical point  $\gamma_c$  for the exact-to-broken  $\mathcal{PT}$  phase transition. Only the real eigenfrequencies is shown for clarity

$\alpha = -0.4$ ,  $\beta = 0.08$  are typical for a diode and they provide a soft on-site nonlinear potential. They can be obtained from a Taylor expansion of the capacitance to voltage relation of an equivalent circuit diode model that gives a very good approximation for weakly driven systems [18, 36].

### 3 Linear eigenfrequency spectra and critical point

In order to obtain the critical value of  $\gamma = \gamma_c$  that separates the exact  $\mathcal{PT}$ -phase, where all the eigenvalues are real, from the broken  $\mathcal{PT}$ -phase, where at least one pair of eigenvalues is complex, we calculate the linear frequency spectrum. This is a straightforward procedure for systems with a relatively small number of SRRs; the roots of the determinant of the linearized Eqs. (1) and (2) for  $\varepsilon_0 = 0$  are obtained with a root-finding algorithm and then plotted against the gain/loss parameter  $\gamma$ . In Figs. 4 and 5, the real eigenfrequencies of  $\mathcal{PT}$ -symmetric metamaterials in both configurations are shown as a function of  $\gamma$ , while the arrows indicate the critical point  $\gamma_c$  in each case. Thus, for  $\gamma < \gamma_c$  all eigenvalues are real, while in the opposite case, at least one pair of eigenvalues has become complex. As we can see from the figures, for  $\gamma > \gamma_c$  more and more eigenfrequency pairs become complex with increasing  $\gamma$ , until they all become complex for a particular value of  $\gamma$ . Moreover, as we



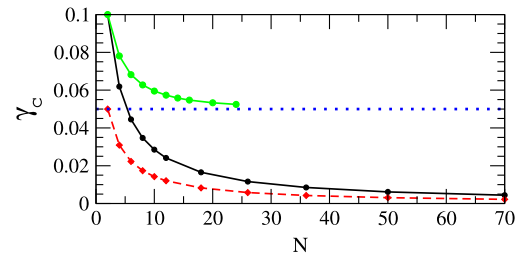
**Fig. 5** Frequency eigenvalues of the free  $\mathcal{PT}$ -symmetric dimer chain as a function of the gain/loss parameter  $\gamma$  for  $\lambda_E = \lambda'_E = 0$ ,  $\lambda_M = -0.1$ ,  $\lambda'_M = -0.05$ , and (a)  $N = 2$ ; (b)  $N = 4$ ; (c)  $N = 8$ ; (d)  $N = 16$ . The arrows indicate the critical point  $\gamma_c$  for the exact-to-broken  $\mathcal{PT}$  phase transition. Only the real eigenfrequencies is shown for clarity

can see from an inspection of Figs. 4 and 5, obtained for the equidistant SRR configuration and the  $\mathcal{PT}$  dimer chain, respectively, the value of  $\gamma_c$  decreases rapidly with increasing number of SRRs  $N$  for the former configuration, while it tends to a constant value for the latter configuration. This can be seen more clearly in Fig. 6, where the critical point  $\gamma_c$  is plotted as a function of  $N$  for both configurations. For the curves corresponding to equidistant SRRs (corresponding to two different values of the magnetic coupling coefficient  $\lambda_M$ ), we see that  $\gamma_c$  is smaller as the magnetic coupling coefficient  $\lambda_M$  lowers. However, in both curves corresponding to equidistant SRRs, the value of the critical point  $\gamma_c$  tends to zero with increasing  $N$ . In contrast, for the  $\mathcal{PT}$  dimer chain configuration, the value of  $\gamma_c$  tends to a constant finite value, which approximately equals the absolute difference of the magnetic coupling coefficients  $\lambda_M$  and  $\lambda'_M$  (see below).

For large systems, we can obtain a condition that determines the critical point  $\gamma_c$  as a function of the magnetic coupling constant(s). In the standard way, we substitute into the linearized Eqs. (1) and (2) for  $\varepsilon_0 = 0$  the trial solutions

$$q_{2n} = A \exp[i(2n\kappa - \Omega\tau)], \quad (3)$$

$$q_{2n+1} = B \exp\{i[(2n+1)\kappa - \Omega\tau]\}, \quad (4)$$



**Fig. 6** Dependence of the critical gain/loss parameter value  $\gamma_c$  on the number of SRRs,  $N$ , for magnetically coupled SRRs in both the equidistant and dimer chain configuration. The black squares and the red diamonds have been calculated for the former configuration with  $\lambda_M = -0.1$  and  $\lambda'_M = -0.05$ , respectively. The green circles have been calculated for the latter configuration with  $\lambda_M = -0.1$ ,  $\lambda'_M = -0.05$ . The lines serve as a guide to the eye

where  $\kappa$  is the normalized wavevector. Then, by requesting nontrivial solutions for the resulting stationary problem, we obtain

$$\Omega_\kappa^2 = (-b \pm \sqrt{b^2 - 4ac})/(2a), \quad (5)$$

where

$$a = 1 - (\lambda_M - \lambda'_M)^2 - \mu_\kappa \mu'_\kappa, \quad (6)$$

$$b = \gamma^2 - 2[1 - (\lambda_E - \lambda'_E)(\lambda_M - \lambda'_M)] + \varepsilon_\kappa \mu'_\kappa + \varepsilon'_\kappa \mu_\kappa, \quad (7)$$

$$c = 1 - (\lambda_E - \lambda'_E)^2 - \varepsilon_\kappa \varepsilon'_\kappa, \quad (8)$$

and

$$\varepsilon_\kappa = 2\lambda_E \cos(\kappa), \quad \varepsilon'_\kappa = 2\lambda'_E \cos(\kappa), \quad (9)$$

$$\mu_\kappa = 2\lambda_M \cos(\kappa), \quad \mu'_\kappa = 2\lambda'_M \cos(\kappa). \quad (10)$$

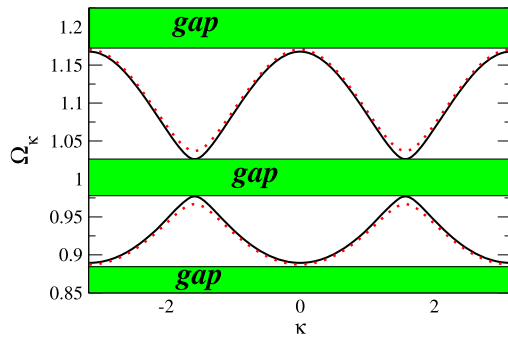
In the following, we neglect the electric coupling between SRRs, i.e.,  $\lambda_E = \lambda'_E = 0$ , for simplicity. Then Eq. (5) reduces to

$$\Omega_\kappa^2 = \frac{2 - \gamma^2 \pm \sqrt{\gamma^4 - 2\gamma^2 + (\lambda_M - \lambda'_M)^2 + \mu_\kappa \mu'_\kappa}}{2(1 - (\lambda_M - \lambda'_M)^2 - \mu_\kappa \mu'_\kappa)}. \quad (11)$$

The condition for having real  $\Omega_\kappa$  for any  $\kappa$  then reads

$$\cos^2(\kappa) \geq \frac{\gamma^2(2 - \gamma^2) - (\lambda_M - \lambda'_M)^2}{4\lambda_M \lambda'_M}. \quad (12)$$

It is easy to see that for  $\lambda_M = \lambda'_M$  corresponding to the equidistant SRR configuration, the earlier condition cannot be satisfied for all  $\kappa$ 's for any positive value of the gain/loss coefficient  $\gamma$ , implying that a large  $\mathcal{PT}$ -symmetric SRR array (Fig. 3, upper panel) will be in the broken phase. To the contrary, for  $\lambda_M \neq \lambda'_M$ , i.e., for a  $\mathcal{PT}$  dimer chain (Fig. 3, lower panel), the above condition is satisfied for all  $\kappa$ 's for



**Fig. 7** Frequency bands for a  $\mathcal{PT}$ -symmetric dimer chain with balanced gain and loss for  $\lambda_M = -0.17$ ,  $\lambda'_M = -0.10$ , and  $\gamma = 0.05$  (black solid);  $\gamma = 0$  (red dotted curves). The gaps are indicated in a green (dark) color

$\gamma \leq \gamma_c \simeq |\lambda_M - \lambda'_M|$ , ( $\gamma^4 \simeq 0$ ). In the exact phase ( $\gamma < \gamma_c$ ), the  $\mathcal{PT}$ -symmetric dimer array has a gapped spectrum with two frequency bands, as shown in Fig. 7. For fixed  $\gamma$ , the width of the gap separating the bands decreases with decreasing  $|\lambda_M - \lambda'_M|$ . For  $\gamma \simeq \gamma_c$  the gap closes, some frequencies in the spectrum acquire an imaginary part and the  $\mathcal{PT}$  metamaterial enters into the broken phase. Note that the gain/loss coefficient  $\gamma$  has little effect on the dispersion curves of the  $\mathcal{PT}$  dimer chain (compare with the dotted curves where  $\gamma$  is set to zero), as long as the sign in front of  $\gamma$  alternates from one SRR to another.

#### 4 Gain-driven breather excitations

For a gapped linear spectrum, large amplitude linear modes become unstable in the presence of driving and nonlinearity. If the curvature of the dispersion curve in the region of such a mode is positive and the lattice potential is soft, large amplitude modes become unstable with respect to formation of DBs in the gap below the linear spectrum [29]. For the parameters used in Fig. 7, the bottom of the lower band is located at  $\Omega_0 \simeq 0.887$ , where the curvature is positive. The corresponding period at the bottom of the lower band is  $T_0 = 2\pi/\Omega_0$ . Moreover, the SRRs are subjected to soft on-site potentials for the selected values of the nonlinear coefficients  $\alpha$  and  $\beta$ . Then DBs can be generated spontaneously by a frequency chirped alternating driver; after turning off the driver, the breathers are driven solely by gain. A similar procedure has been applied successfully to lossy nonlinear metamaterials with a binary structure [16, 17, 24]. The results are illustrated in Figs. 8 and 9, where the case of a slight imbalance between gain and loss and its effect on breather generation has been also considered. In these figures, a density plot of the local energy  $E_n$  of a  $\mathcal{PT}$ -symmetric metamaterial is shown on the  $n$ - $\tau$  plane for two different values of the driving amplitude  $\varepsilon_0$ .

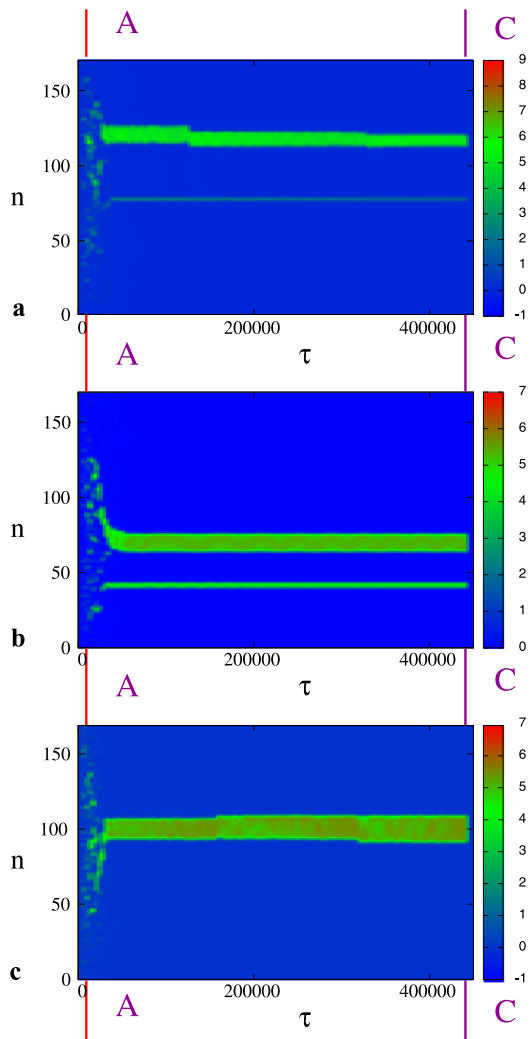
In the following, Eqs. (1) and (2) implemented with the boundary conditions

$$q_0(\tau) = q_{N+1}(\tau) = 0, \quad (13)$$

that accounts for the termination of the structure in finite systems, are integrated with a fourth-order Runge–Kutta algorithm with a fixed time-step. In order to prevent instabilities that will result in divergence of the energy at particular sites in finite time, we consider a longer dimer chain with total number of SRRs  $N + 2N_\ell$ ; then we replace the gain with equivalent amount of loss at exactly  $N_\ell$  SRRs at each end of the extended chain. In other words, we embed the  $\mathcal{PT}$ -symmetric dimer chain into a geometrically identical lossy chain, in order to help the excess energy to go smoothly away during evolution, living behind stable (or at least very long-lived) breather structures. We use the following procedure described in detail in [19]:

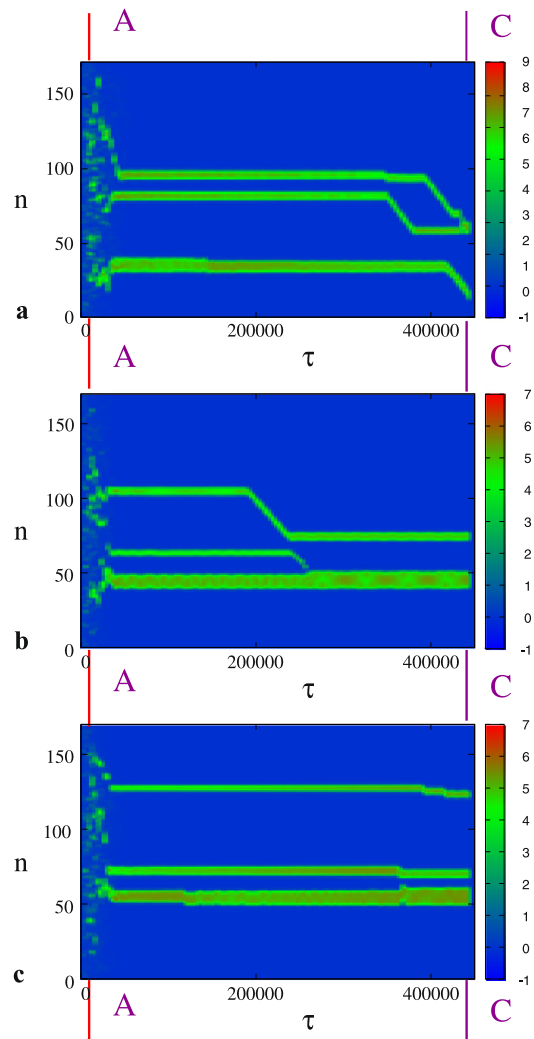
- At time  $\tau = 0$ , we start integrating Eqs. (1) and (2) from zero initial state without external driving for  $500T_0 \simeq 3500$  time units (t.u.) to allow for significant development of large amplitude modes.
- At time  $\tau \simeq 3500$  t.u., the driver is switched-on with low-amplitude  $\varepsilon_0$  and frequency slightly above  $\Omega_0$  ( $1.01\Omega_0 \simeq 0.894$ ). The frequency is then chirped downward with time to induce instability for the next 10600 t.u. ( $\sim 1500T_0$ ), until it is well below  $\Omega_0$  ( $0.997\Omega_0 \simeq 0.882$ ). During that phase, a large number of excitations are generated that move and strongly interact to each other, eventually merging into a small number of high amplitude breathers and multibreathers.
- At time  $\tau \simeq 14100$  t.u. (point A on Figs. 8 and 9), the driver is switched off and the DBs that have been formed are solely driven by the gain. They continue to interact for some time until they reach an apparently stationary state and get trapped at particular sites. The high density segments between the points A and C in Figs. 8 and 9 precisely depict those gain-driven DB structures.
- At time  $\tau \sim 440000$  t.u. (point C on Figs. 8 and 9), the gain is replaced everywhere by equal amount of loss, and the breathers die out rapidly.

Note that the above procedure of breather generation is very sensitive to parameter variations of the external fields. Even though the values of the driving amplitudes in Figs. 8 and 9 are rather close (i.e.,  $\varepsilon_0 = 0.085$  and  $0.095$ , respectively), the breather structures as well as their numbers are different. In Fig. 8(b), in the balanced gain/loss case, we observe two distinct structures that have been formed that correspond to a relatively high amplitude multibreather and a low amplitude breather. These structures remain stationary during the long time interval they have been followed ( $>56000T_0$ ). In Figs. 8(a) and 8(c), gain and loss are not perfectly matched; in Fig. 8(a), loss exceeds gain by a small



**Fig. 8** Spatiotemporal evolution of the energy density  $E_n$  for a  $\mathcal{PT}$ -symmetric dimer chain with  $N = 70$ ,  $N_\ell = 10$ ,  $\Omega_0 = 0.887$ ,  $\gamma = 0.002$ ,  $\lambda_M = -0.17$ ,  $\lambda'_M = -0.10$  ( $\lambda_E = \lambda'_E = 0$ ),  $\varepsilon_0 = 0.085$ ,  $\gamma = 0.002$  and (a) excess loss 0.2 %; (b) balanced case; (c) excess gain 0.2 %

amount while in Fig. 8(c) gain exceeds loss by the same small amount. Notably, breather excitations may still be formed through the frequency chirping procedure in the presence of a small amount of either net gain or net loss. Indeed, as we may observe comparing Figs. 8(a) and 8(c) with Fig. 8(b), the same structures are formed [except the low amplitude breather that is not visible in Fig. 8(c)]. When loss exceeds gain [Fig. 8(a)] the multibreather losses its energy at a low rate, with its excited sites that are closer to its end-points gradually falling down to a low amplitude state. Similarly, when gain exceeds loss [Fig. 8(c)], the high amplitude multibreather slowly gains energy and becomes wider. In both cases, breather destruction will take place in a time-scale that depends exponentially on the gain/loss imbalance. Thus, in an experimental situation, where gain/loss



**Fig. 9** Spatiotemporal evolution of the energy density  $E_n$  for a  $\mathcal{PT}$ -symmetric dimer chain with  $N = 70$ ,  $N_\ell = 10$ ,  $\Omega_0 = 0.887$ ,  $\gamma = 0.002$ ,  $\lambda_M = -0.17$ ,  $\lambda'_M = -0.10$  ( $\lambda_E = \lambda'_E = 0$ ),  $\varepsilon_0 = 0.095$ ,  $\gamma = 0.002$  and (a) excess loss 0.2 %; (b) balanced case; (c) excess gain 0.2 %

balance is only approximate, it will be still possible to observe breathers at relatively short time-scales.

Similar observations hold for Fig. 9 as well. In this figure, we observe three relatively high amplitude multibreather structures that are formed both in the balanced [Fig. 9(b)] and the imbalanced case [Fig. 9(a) and Fig. 9(c), for net loss and gain, respectively]. Here, we also observe that instabilities may appear even after long time intervals of apparently stationary breather evolution. Whenever this happens, DBs start moving through the lattice until they get once more trapped at different lattice sites. In Fig. 9(b), such an instability appears between 200000–250000 t.u. for the two narrower multibreather structures. The one of them gets trapped a few tenths lattice sites away from its previous position, while the other (the narrowest) collides and it is absorbed by the wide multibreather located at  $n \sim 50$ .



## 5 Classical $\mathcal{PT}$ -symmetry in zero dimensions

In the classical domain, in all cases of  $\mathcal{PT}$ -symmetric systems investigated so far, the combination of time-reversal and parity symmetries is utilized: In a given time-evolution, if we reverse time while “reflecting” position and momentum, we must retrace the original path. The parity operation requires that the system is extended either in continuous or discrete space in order to be able to perform this operation. We show here that this is not necessary and that the features of the  $\mathcal{PT}$ -symmetric systems can be preserved in “zero” dimensions where the parity symmetry is trivial.

We consider the following simple harmonic oscillator:

$$\ddot{x} + 2\theta(t)\dot{x} + \omega_0^2 x = 0, \quad (14)$$

where  $x \equiv x(t)$  is the equilibrium displacement of a mass (the charge in an  $RLC$  circuit),  $\omega_0$  the resonant oscillator frequency while  $\theta(t)$  is a time-dependent “damping” term; both  $\omega_0$  and  $\theta(t)$  are scaled to the mass (impedance of the circuit). We take  $\theta(t)$  to be periodic with period  $T$ , viz.  $\theta(t + T) = \theta(t)$  while its values may be both positive and negative, i.e., for some part of the period the oscillator experiences damping while in the rest of the period time amplification, or anti-damping. We investigate the oscillator evolution after long time and the stability of the motion. Instead of addressing a general periodic function  $\theta(t)$ , we focus on a simple form that makes the problem readily solvable, viz. we take

$$\theta(t) = \begin{cases} +\gamma & \text{if } 0 \leq t < \tau_1, \\ -\gamma & \text{if } \tau_1 \leq t < \tau_2, \end{cases} \quad (15)$$

where  $T = \tau_1 + \tau_2$  and taking the plus (minus) sign in front of the coefficient  $\gamma$  ( $\gamma$  is defined as a positive constant,  $\gamma > 0$  that may assume any value between zero and unity) we have in the first (second) part of the cycle loss (gain). With this form of piece-wise constant function  $\theta(t)$ , we can easily solve Eq. (14) for the loss (L) segment of time duration  $\tau_1$  and gain (G) segment of duration  $\tau_2$ . The form of Eq. (15) permits to view the problem as mapping of the position-velocity vector at a given time to the position-velocity vector at a later time; if in the beginning of the gain (loss) period (assuming  $t = 0$ ) we have position and velocity equal to  $(x_0, \dot{x}_0)$ . Then after the evolution during time  $\tau$  ( $\tau_1$  or  $\tau_2$ , respectively) we obtain:

$$\begin{pmatrix} x \\ \dot{x} \end{pmatrix} = M_{G/L}(\tau) \begin{pmatrix} x_0 \\ \dot{x}_0 \end{pmatrix} \quad (16)$$

where for gain we have

$$M_G(\tau_1) = \frac{e^{\gamma\tau_1}}{\delta}$$

$$\times \begin{pmatrix} \delta \cos \delta\tau_1 - \gamma \sin \delta\tau_1 & \sin \delta\tau_1 \\ -\omega_0^2 \sin \delta\tau_1 & \delta \cos \delta\tau_1 + \gamma \sin \delta\tau_1 \end{pmatrix} \quad (17)$$

and for the loss, respectively,

$$M_L(\tau_1) = \frac{e^{-\gamma\tau_2}}{\delta} \times \begin{pmatrix} \delta \cos \delta\tau_2 + \gamma \sin \delta\tau_2 & \sin \delta\tau_2 \\ -\omega_0^2 \sin \delta\tau_2 & \delta \cos \delta\tau_2 - \gamma \sin \delta\tau_2 \end{pmatrix} \quad (18)$$

where  $\delta = \sqrt{\omega_0^2 - \gamma^2}$ . Using the mapping, we may obtain long time evolution after  $N$  periods  $T$  as a repetitive application of the matrices  $M_G(\tau_1)$  and  $M_L(\tau_2)$  to an arbitrary initial state  $(x_0, \dot{x}_0)$ . Since the matrices  $M_{L/G}(\tau)e^{\pm\gamma\tau}$  are unimodular, the long time evolution will be dominated by the exponential term  $\exp[N\gamma(\tau_1 - \tau_2)]$ ; this leads trivially to exponential growth ( $\tau_1 > \tau_2$ ) or exponential decay ( $\tau_1 < \tau_2$ ). As a result, we consider the more interesting case with  $\tau_1 = \tau_2 = \tau \equiv T/2$ ; in this case the gain and loss power is perfectly matched during the period  $T$ . The combined propagation matrix after one period (assuming first gain) is simply  $M(T) = M_L(\tau)M_G(\tau)$ , i.e.,

$$M(T) = \frac{1}{\delta^2} \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \quad (19)$$

where  $M_{ij}$  are given by

$$M_{11} = -\gamma^2 + \omega_0^2 \cos(2\phi), \quad (20)$$

$$M_{12} = +2 \sin \phi (\delta \cos \phi + \gamma \sin \phi), \quad (21)$$

$$M_{21} = -2\omega_0^2 \sin \phi (\delta \cos \phi - \gamma \sin \phi), \quad (22)$$

$$M_{22} = -\gamma^2 + \omega_0^2 \cos(2\phi) \quad (23)$$

and  $\phi = \delta\tau \equiv \delta T/2$ . The matrix  $M$  is clearly also unimodular with eigenvalues  $e^{i\mu}$  and  $e^{-i\mu}$ ; since the trace of a matrix is invariant we find

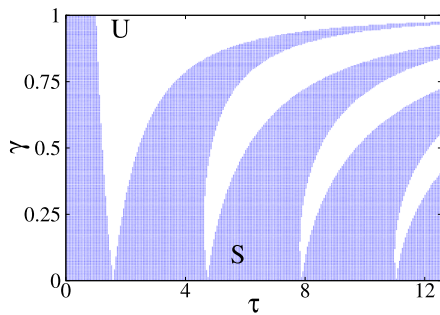
$$\cos \mu = \frac{-\gamma^2 + \omega_0^2 \cos 2\phi}{\delta^2}. \quad (24)$$

**Stability equation** Equation (24) can be rewritten as

$$\cos \mu = \frac{1 - B^2 \cos 2\phi}{1 - B^2} = 1 + \frac{2B^2 \sin^2 \phi}{1 - B^2} \quad (25)$$

with  $B = \frac{\omega_0}{\gamma}$ . In order to have stable motion, it is necessary that  $|\cos \mu| \leq 1$ , or  $-1 \leq 1 + \frac{2B^2 \sin^2 \phi}{1 - B^2} \leq 1$ , leading to

$$-2 \leq \frac{2B^2 \sin^2 \phi}{1 - B^2} \leq 1. \quad (26)$$



**Fig. 10** Phase diagram on the  $\gamma$ - $\tau$  plane for the harmonic oscillator with time-dependent “damping” term, obtained from Eq. (29). The stability region is indicated in a blue (dark) color

Equation (26) has solutions only for  $|B| > 1$  or  $|\gamma| < \omega_0$ , for  $\omega_0 > 0$ ; in the latter case, we find

$$|\cos \phi| \geq \left| \frac{\gamma}{\omega_0} \right|. \quad (27)$$

The range thus of allowed values for the angle  $\phi$  ( $\gamma > 0$ ) is

$$\begin{aligned} \frac{\gamma}{\omega_0} &\leq \cos \phi \leq 1, \\ -1 &\leq \cos \phi \leq -\frac{\gamma}{\omega_0}. \end{aligned} \quad (28)$$

We note that there are multiple allowed solutions marked by the lines  $\cos \phi = \pm \gamma/\omega_0$ , i.e., for the three parameters of the problem  $\gamma$ ,  $T = 2\tau$  and  $\omega_0$ , the transcendental equation

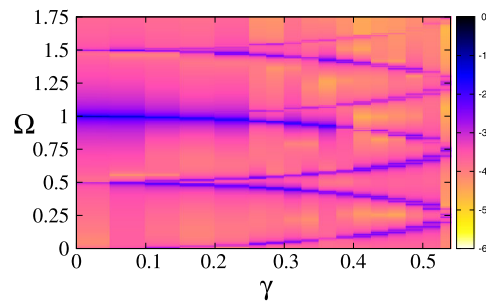
$$\cos(\delta\tau) = \begin{cases} +\frac{\gamma}{\omega_0} & \text{for } 2n\pi - \pi/2 < \delta\tau < 2n\pi + \pi/2, \\ -\frac{\gamma}{\omega_0} & \text{for } 2\pi n + \pi/2 < \delta\tau < 2\pi n + 3\pi/2, \end{cases}$$

where  $n = 0, \pm 1, \pm 2, \dots$ , marks the onset of the transition from stable to unstable evolution. This is the equivalent to the  $\mathcal{PT}$  transition from the exact (stable) to the broken (unstable) phase in this zero-dimensional problem. Using Eq. (27), we construct a  $\mathcal{PT}$  phase diagram on the  $\tau$ - $\gamma$  plane (Fig. 10), where the blue (dark) color indicates regions of stability. If we fix one of the parameters, the variation of the other drives the oscillator through alternating stable and unstable regions, as can be readily observed from Fig. 10.

Introducing the frequency  $\omega = 2\pi/T \equiv \pi/\tau$ , we define the reduced parameters  $\Omega = \omega/\omega_0$  and  $\tilde{\gamma} = \gamma/\omega_0$ . Then the equation that controls the stability regions becomes

$$\left| \cos \left[ \frac{\pi \sqrt{1 - \gamma^2}}{\Omega} \right] \right| = \gamma, \quad (29)$$

where the tilde has been dropped for simplicity. Equation (29) has solutions for  $|\gamma| < 1$ ; for different reduced frequencies  $\Omega$  we obtain different number of solutions of the earlier equation, the number of the latter increases with decreasing frequency  $\omega$ . Once we have the solutions of Eq. (29), we can



**Fig. 11** Density plot of the logarithm of the frequency spectra of  $x(t)$ ,  $y = \log_{10}\{PS[x(t)]\}$ , as a function of  $\gamma$ . The discrete frequency components of the spectra for each value of  $\gamma$  are indicated with a blue (darker) color

find the regimes of stability and instability. Consider the resonant case  $\Omega = 1$  where the external frequency of gain/loss alternation matches the self-frequency of the oscillator. Besides the trivial solution at  $\gamma = 0$ , the numerical solution of Eq. (29) gives  $\gamma_1 \approx 0.676$  so that the stable region is in the range  $0 \leq \gamma \leq \gamma_1$ . For  $\Omega = 0.5$ , the corresponding solutions are  $\gamma_1 \approx 0.54$ ,  $\gamma_2 \approx 0.80$ , and  $\gamma_3 \approx 0.90$  with two stability regions, i.e.,  $0 \leq \gamma \leq \gamma_1$  and  $\gamma_2 \leq \gamma \leq \gamma_3$ .

The stable solutions of Eq. (14) as a function of time  $t$  are in general quasiperiodic oscillations whose spectral content varies both with  $\tau$  and  $\gamma$ . For an illustration, we consider a particular value of  $\tau$ , i.e.,  $\tau = 2\pi$  ( $\Omega = 0.5$ ) for which the boundaries of the stability regions have been calculated above. For the interval with relatively low values of  $\gamma$ ,  $0 \leq \gamma \leq \gamma_1 \approx 0.54$ , that is more physically relevant, we present a density plot of the logarithm of the frequency spectra of  $x(t)$ ,  $y = \log_{10}\{PS[x(t)]\}$ , as a function of  $\gamma$  (Fig. 11). In this figure, the discrete frequency components of the spectra for each value of  $\gamma$  are indicated in dark (blue) color. For  $\gamma = 0$  and very close to zero, the only frequency appearing in the spectrum is the eigenfrequency of the oscillator  $\Omega \approx 1$ . With increasing  $\gamma$ , the frequency components at  $\Omega \approx 1 \pm 0.5$  become more and more important. At about  $\gamma = 0.15$ , these half-integer frequency components start splitting into pairs of frequencies that are symmetric around the half-integer values. The separation between these pairs increases with further increasing  $\gamma$ , and the frequency components from neighboring pairs come closer and closer together until they eventually merge for  $\gamma$  approaching its critical value  $\gamma_1 \approx 0.54$ .

## 6 Conclusions

We have investigated theoretically a  $\mathcal{PT}$ -symmetric nonlinear metamaterial relying on gain and loss. Eigenfrequency spectra for linearized systems of either small and large  $N$  and two different configurations were calculated and the critical points  $\gamma_c$  were determined. Large  $\mathcal{PT}$ -symmetric

metamaterials with the dimer chain configuration exhibit phase transitions for the exact to the broken  $\mathcal{PT}$ -symmetry phase, while large  $\mathcal{PT}$ -symmetric metamaterials with the equidistant SRR configuration are always in the broken  $\mathcal{PT}$  phase.

In the presence of nonlinearity, we have demonstrated numerically the a  $\mathcal{PT}$ -symmetric dimer chain supports localized excitations in the form of discrete breathers. Breathers are excited by a purely dynamical process, with a frequency chirped external magnetic field that induces instability in a zero initial state. Subsequently, the nonlinearity focuses energy around points that have acquired high amplitude leading to the formation of localized structures. The external field is then switched off and those localized structures are then solely driven by the gain, the excess energy lives the system through its lossy parts at the ends, leading eventually to breather generation.

Remarkably, slight imbalance between gain and loss does not destroy the breathers instantly; they can still be generated through the frequency chirping procedure and they can be regarded as stationary for relatively short time intervals. In the long term, the imbalanced breathers either gain constantly energy and diverge or constantly lose energy and vanish. The time-scale for the latter events depends exponentially from the amount of imbalance.

We have introduced a “zero-dimensional”  $\mathcal{PT}$  system that can be realized by a harmonic oscillator with a “damping” term that provides balanced gain and loss, through alternation of the sign of the damping coefficient. We consider a piecewise linear gain/loss function and obtain a stability condition, i.e., a relation between the parameters of the problem. We thus obtain a “phase diagram” with parameter regions where oscillatory (stable) motion and diverging (unstable) motion occur; by crossing the stability boundary marks, the onset of the transition from stable to unstable evolution that is equivalent to the  $\mathcal{PT}$  transition from the exact to the broken phase in this zero-dimensional problem.

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